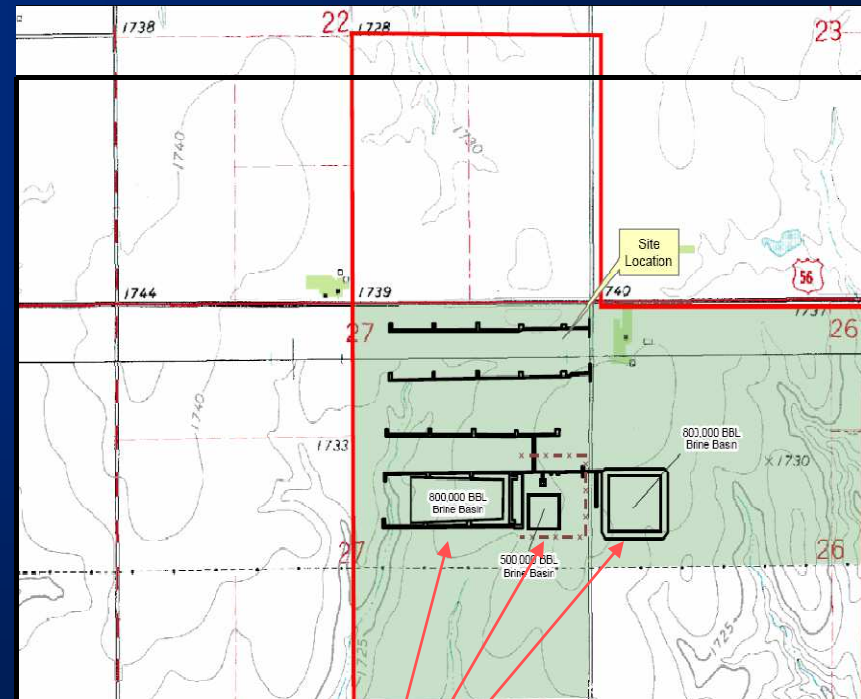


Proving the Effectiveness of Interceptor Trench for Hydraulic Containment of Chloride Impacted Groundwater at a Natural Gas Liquid Storage Facility, South Central Kansas, USA

Jeffrey Binder, PG
Burns & McDonnell Engineering Company



Site Location Map



Brine
Ponds

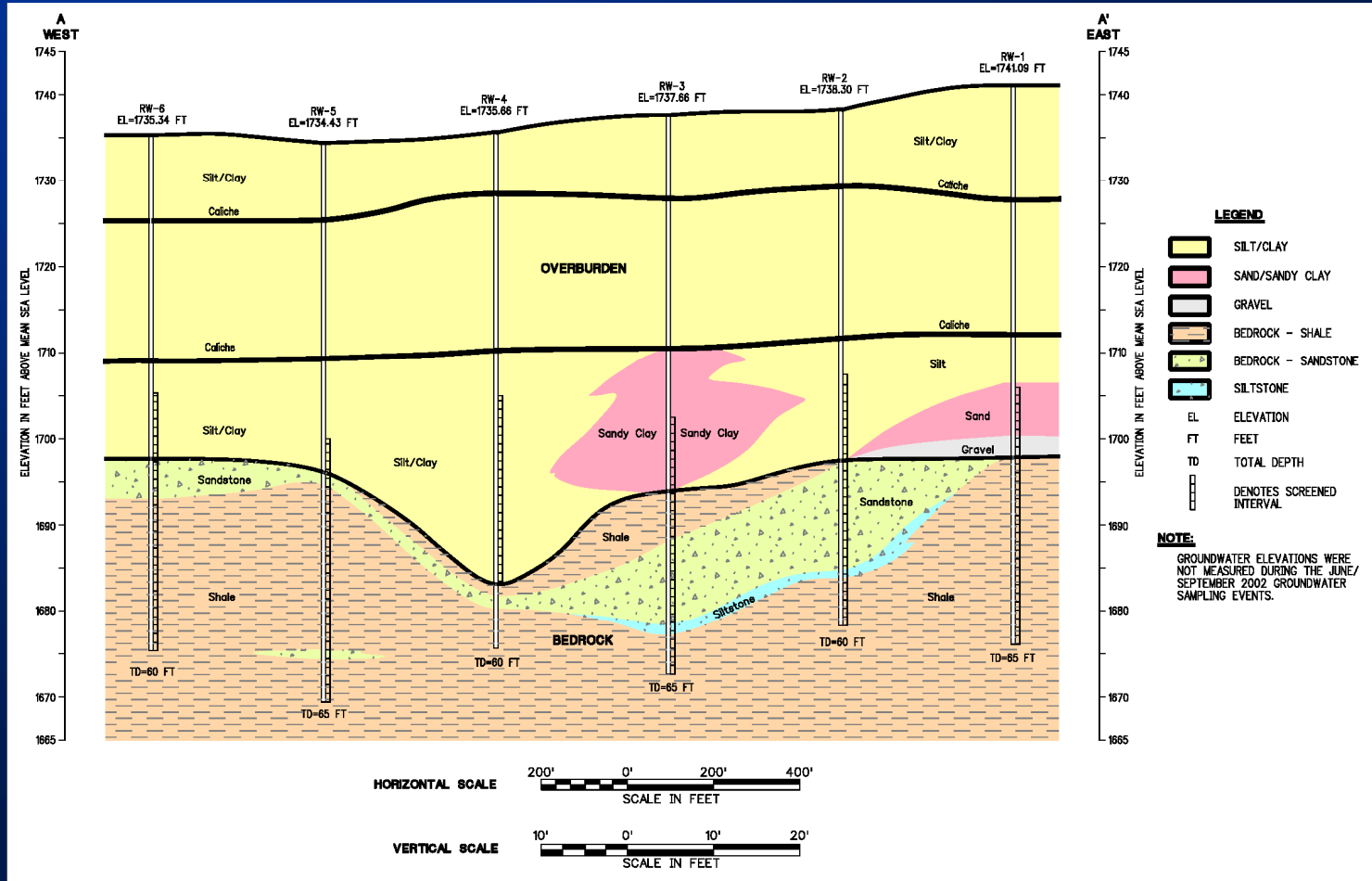
Site Overview

- Located in rural south central Kansas
- Natural gas liquid (NGL) storage facility with brine storage ponds
- NGL stored in salt caverns 700 ft. bgs
- Groundwater contamination as a result of release from previously unlined brine ponds
- Chloride concentrations in excess of acceptable levels (SMCL 250 mg/L)

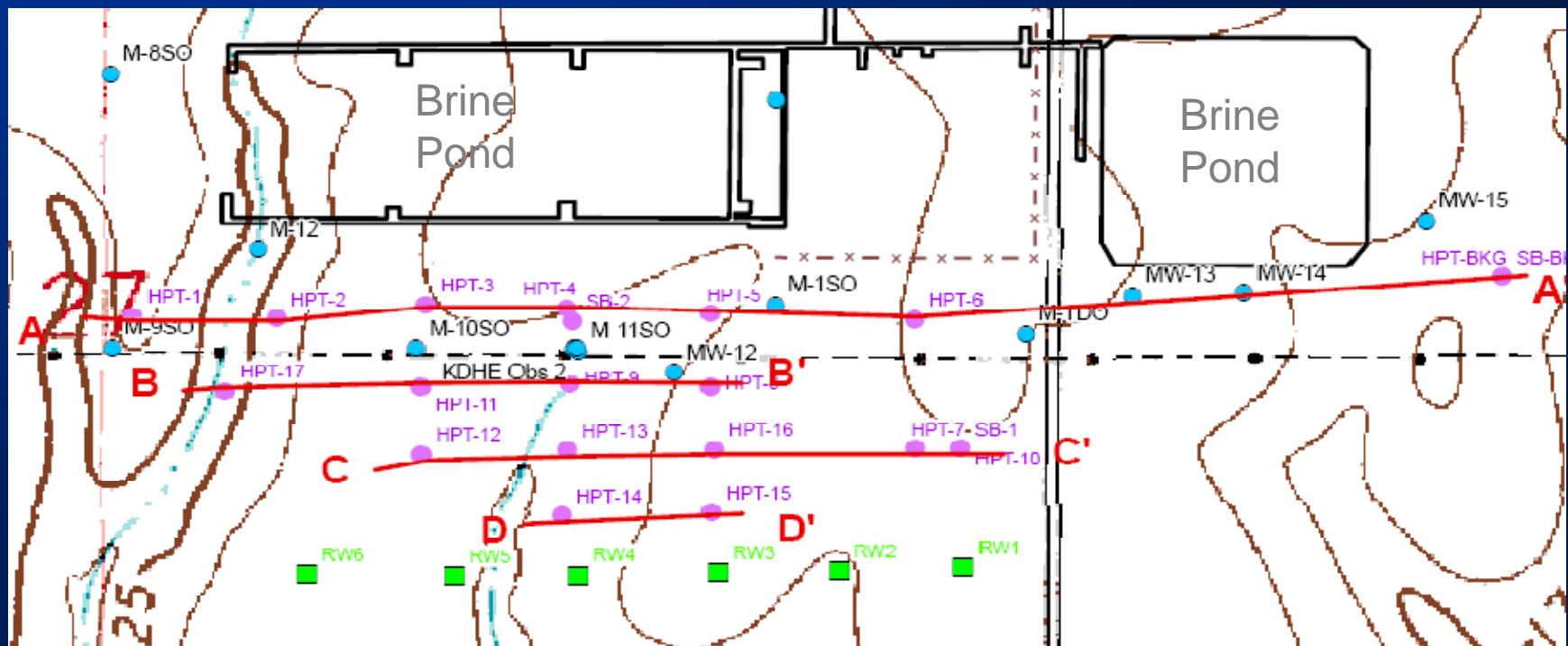
Geology and Hydrogeology

- Site consists of loess overburden deposits
- The uppermost bedrock consists of shale, siltstone and sandstone of the Cretaceous Kiowa Shale
- Groundwater yield to wells is limited to 0.25 to 1.5 gpm
- Groundwater movement controlled by flow along preferential pathway in soil and bedrock
- Relatively tight soil/rock matrix

Generalized Geologic Profile



HPT Locations and Profile Lines

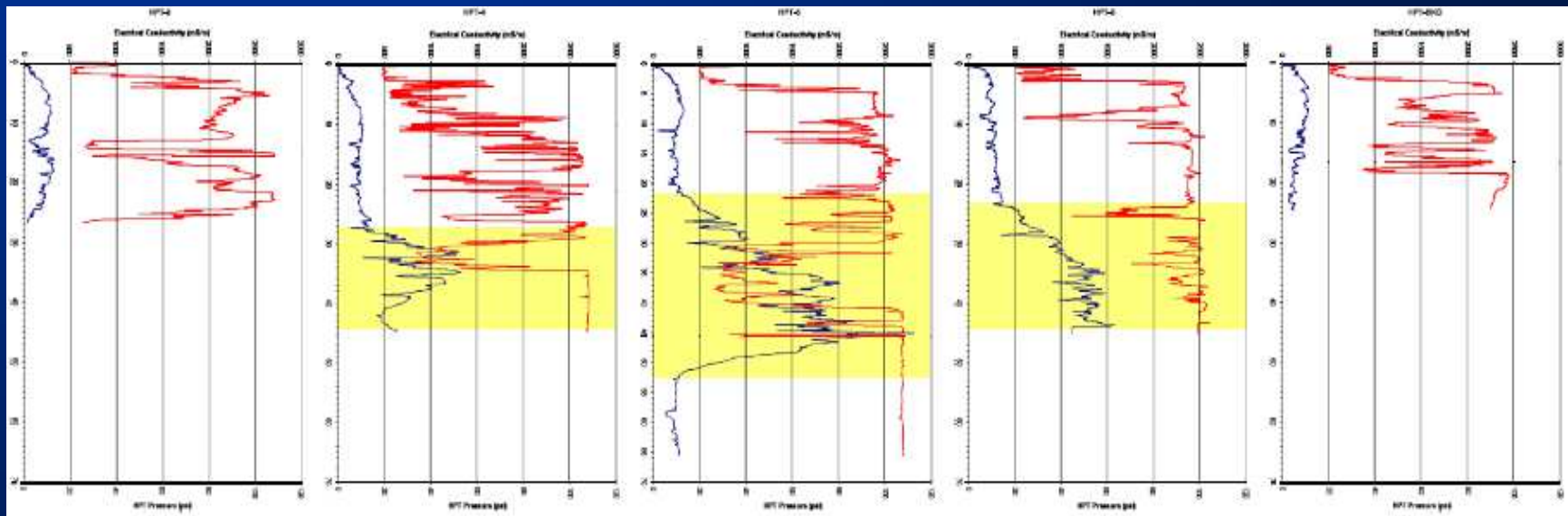


500 0 500 Feet

- Monitoring Well
- HPT Survey
- Recovery Well
- A' Profile Line



HPT Profile A-A'



LEGEND



CHLORIDE IMPACT

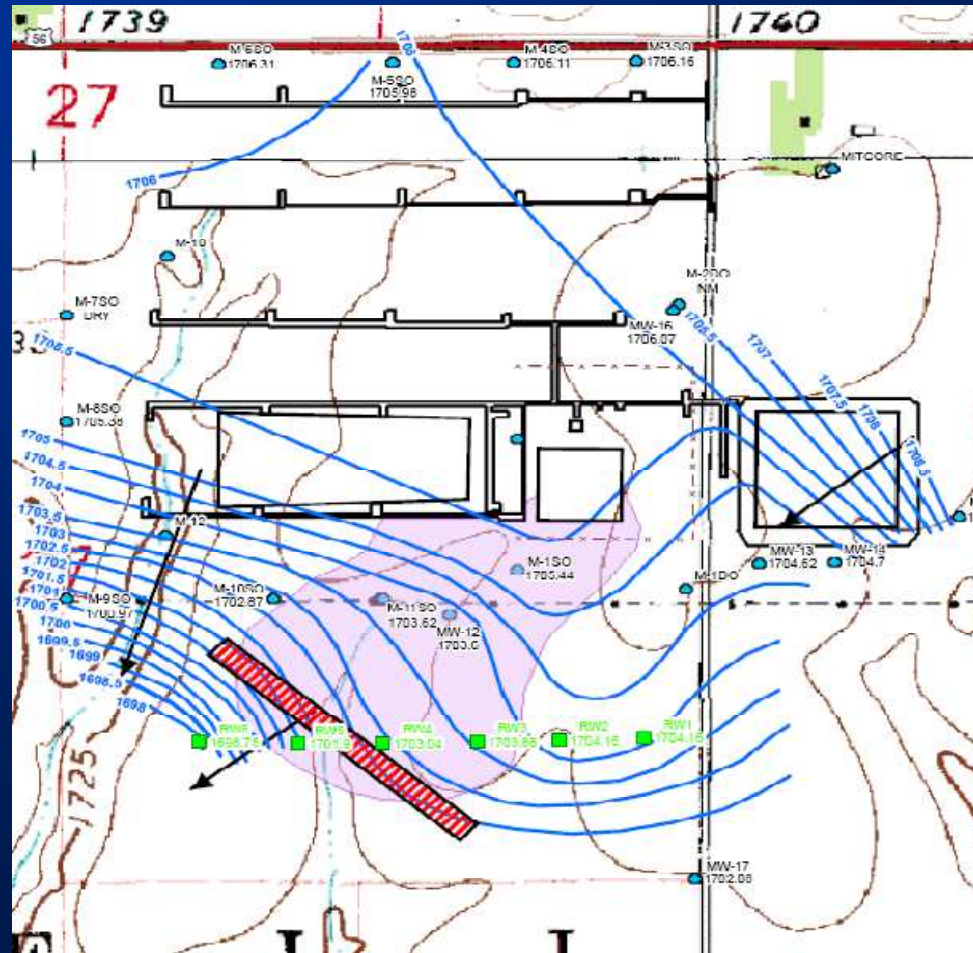


ELECTRICAL CONDUCTIVITY (EC)



HYDRAULIC PROFILLING TOOL (HPT)

Potentiometric Surface



LEGEND

- Monitoring Well
- Recovery Well
- Groundwater Elevation Contour
- Groundwater Flow Direction
- Proposed Trench
- Chloride Impact

Hydrogeologic Testing

- Historically several attempts to perform pump tests in vertical wells
- Previous tests indicated yields between 0.25 to 1.5 gpm
- ROI was 10 to 30 feet
- Evaluation led to installation of the collection trench as hydraulic containment alternative to maximize the interconnection of preferential groundwater flowpaths

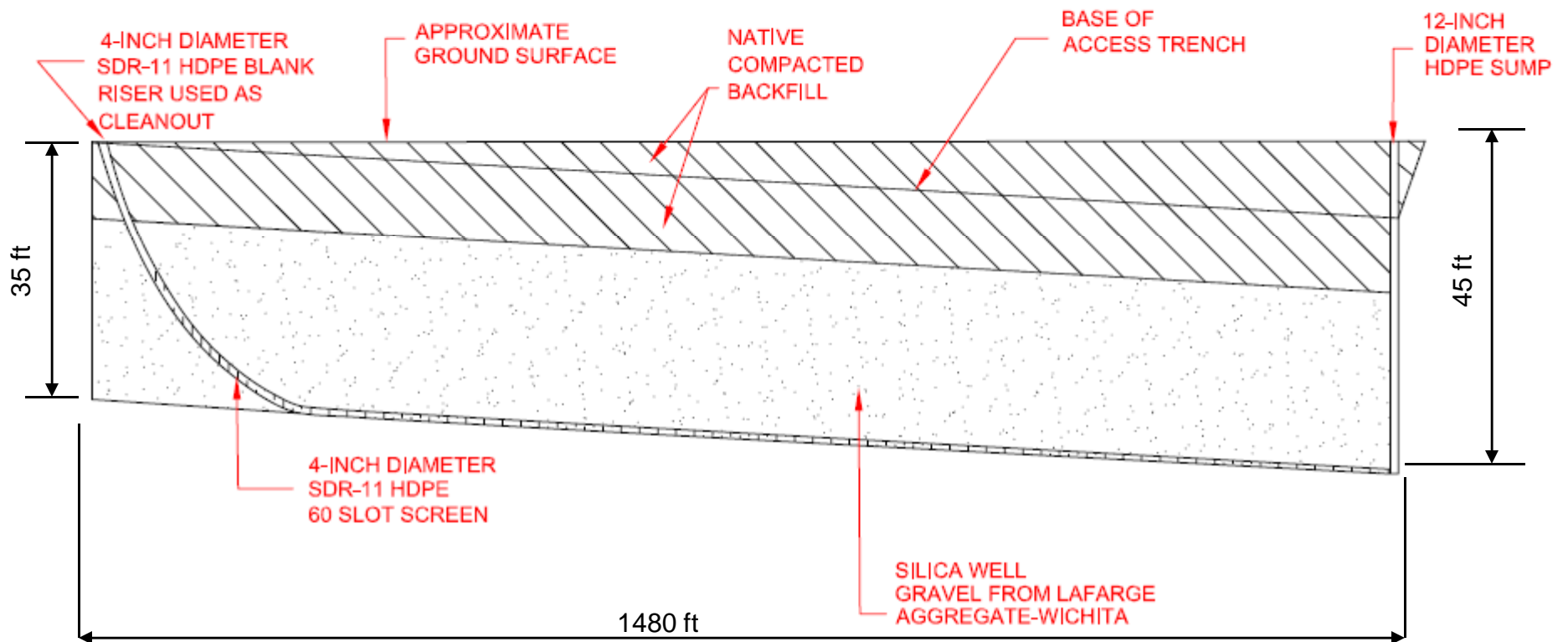
OnePass Trencher



Trench Construction



Trench Installation



Groundwater Recharge



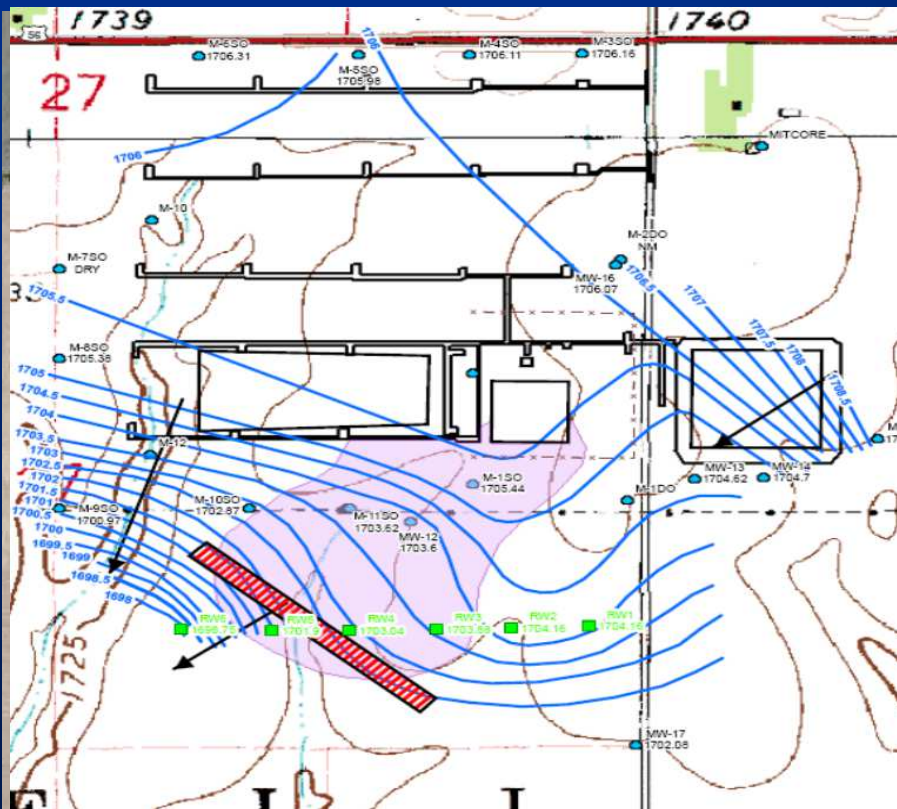
- Following installation of trench the question arose as to the estimated yield for design of the collection and treatment system
- Client wasn't interested in aquifer testing
- End result was to use existing data and SWAG approx. yield and pumping rate
- Maximum rate was 10 gpm with operation at around 8 gpm (system installed 2007-2008)

Concerns

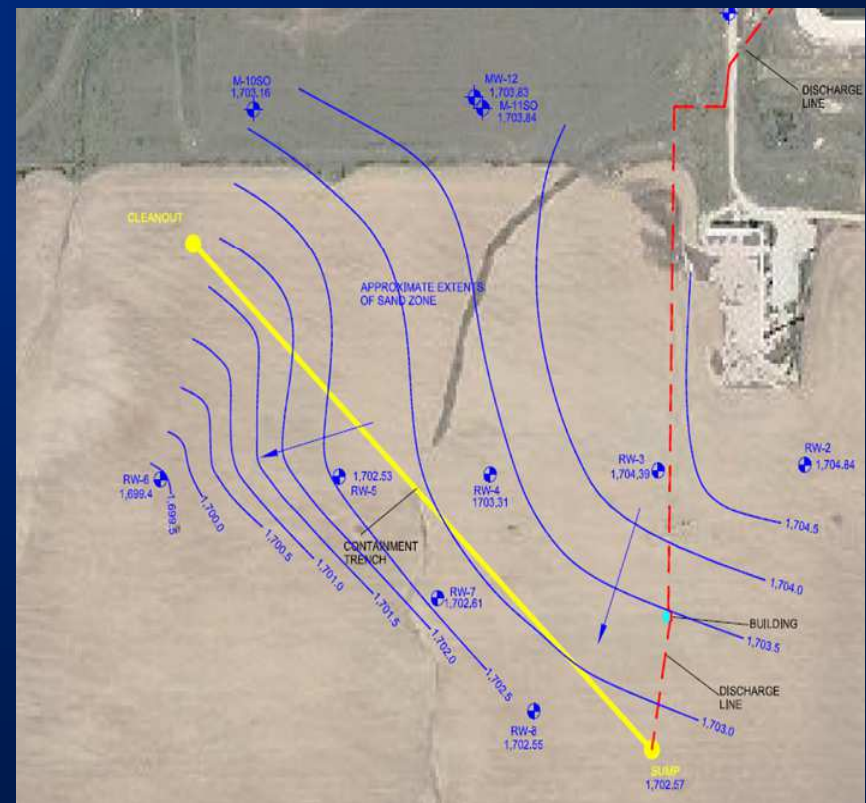
- System didn't provide capture and only provided minimal recovery of impacted fluids
- Regulators were not satisfied with the lack of hydraulic containment/control
- Requested that aquifer testing be performed to prove or disprove effectiveness of trench

Comparison Pumping vs. Static

Static Condition 2006

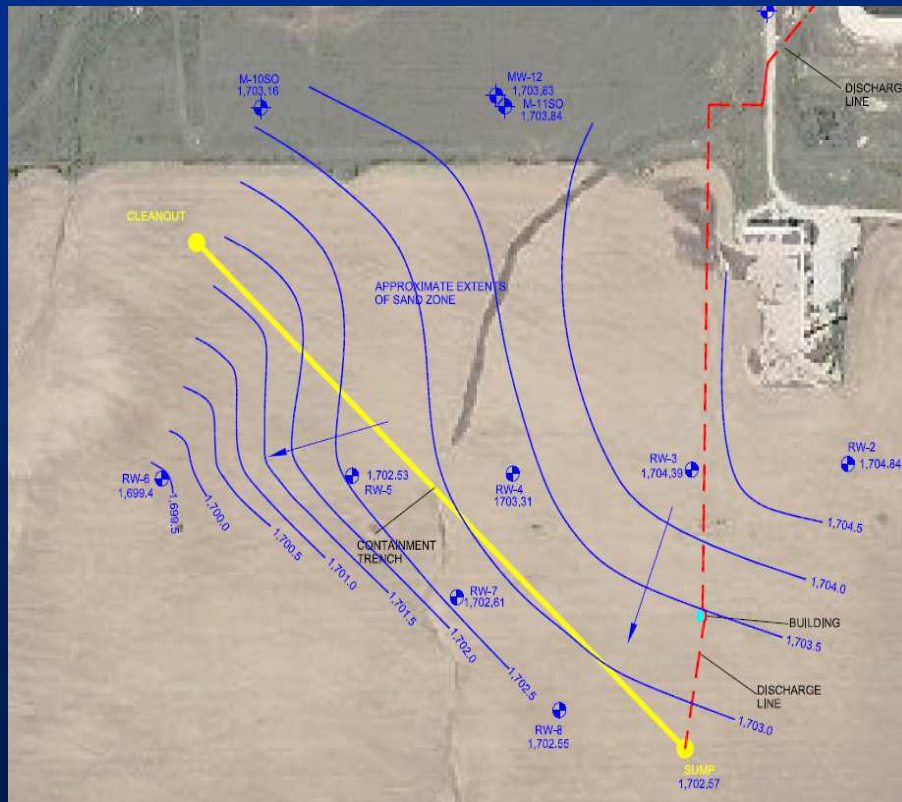


Pumping Condition 2010

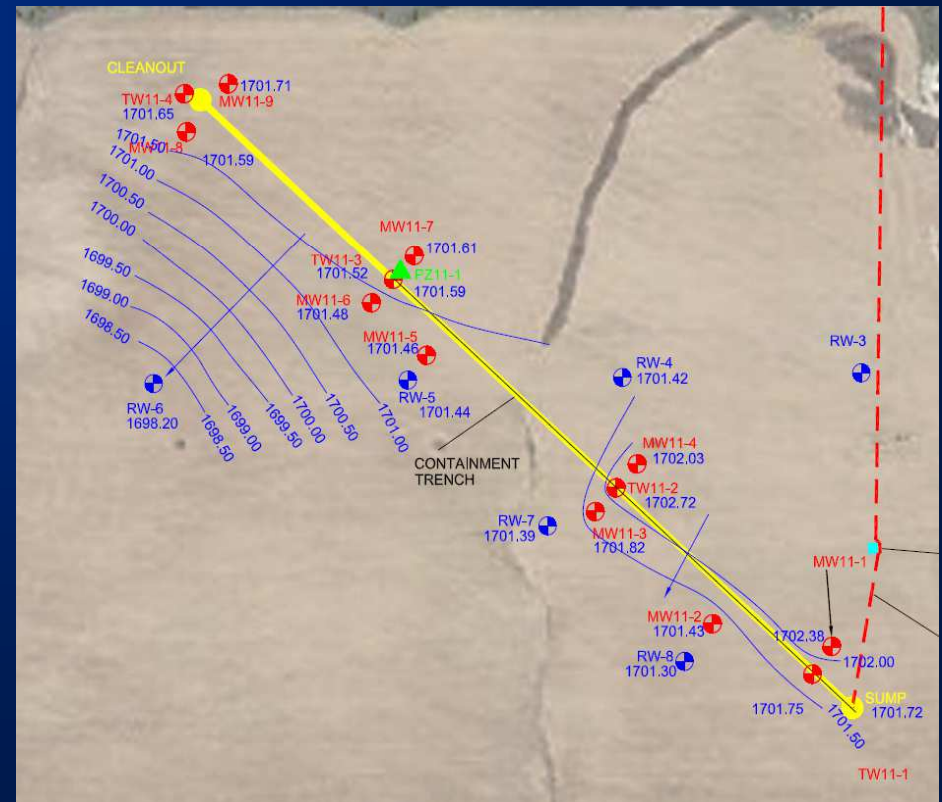


Comparison Pumping vs. Static

Pumping Condition 2010



Static Condition 2012



Field Activities

- Series of piezometers and monitoring wells were installed (four inside and nine outside trench)
- Step test performed (40, 60, 80, & 93 gpm). 50 gpm selected for constant rate
- 76 hour constant rate test

Trench Profile

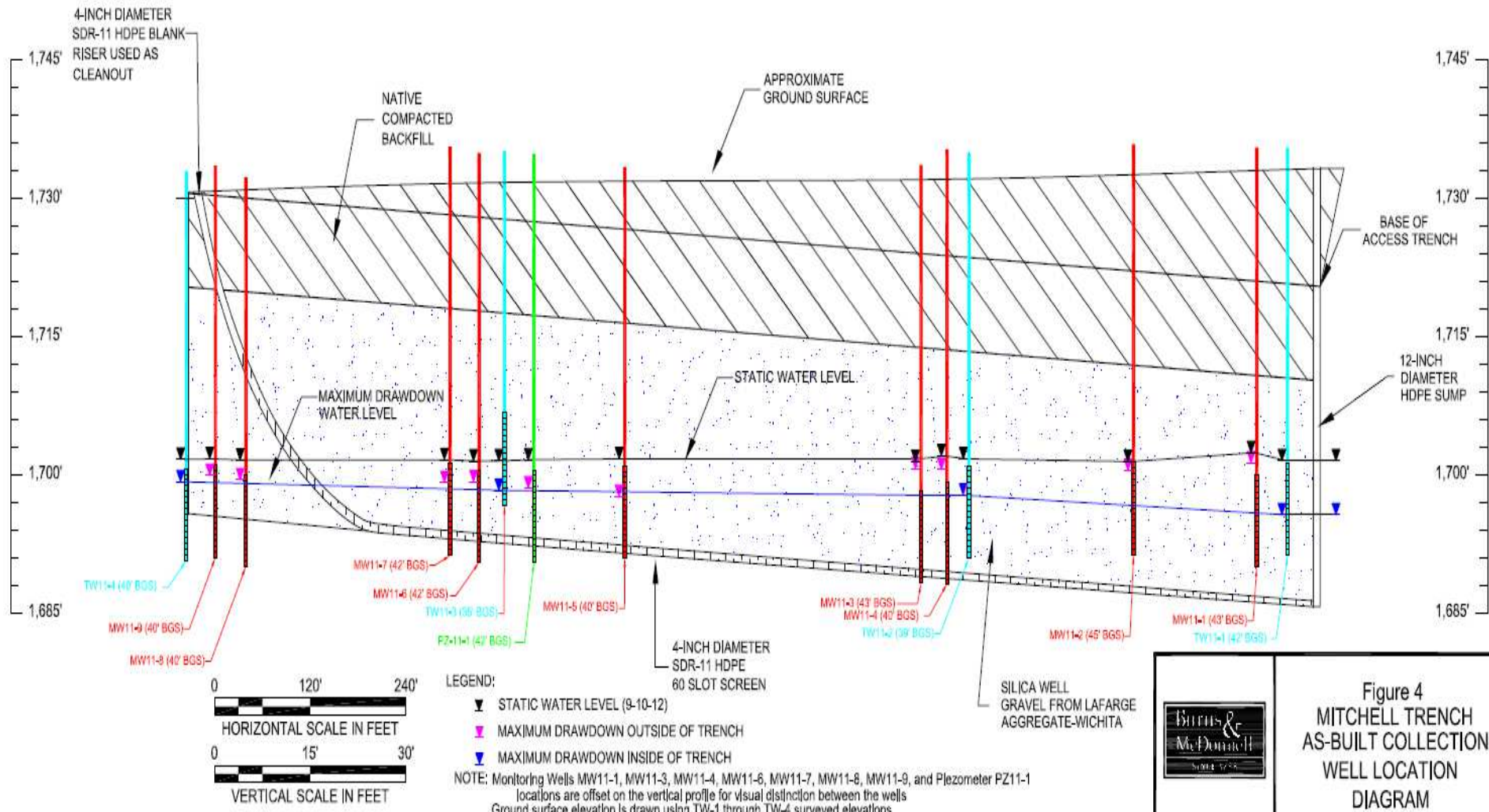
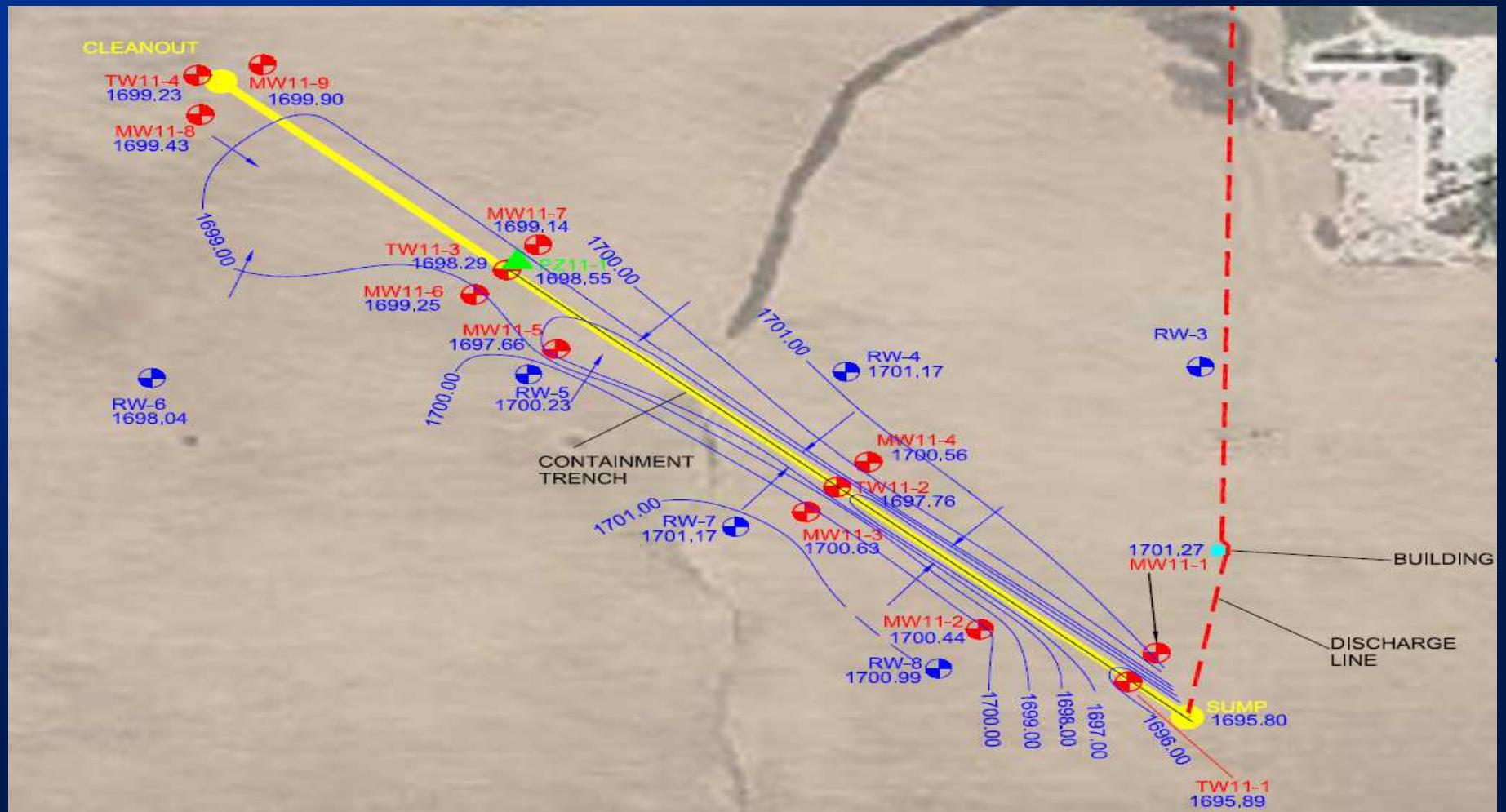


Figure 4
MITCHELL TRENCH
AS-BUILT COLLECTION
WELL LOCATION
DIAGRAM



Maximum Drawdown – 2012 Test



Findings

- Aquifer saturated thickness = 16.33 ft
- Drawdown observed along trench (ranged from 1.8 ft. (cleanout) to 5.9 ft (sump))
- Hydraulic conductivity $E10^{-1}$ cm/s (trench) and $E10^{-2}$ to $E10^{-4}$ cm/s (outside trench)
- Influence and capture observed within and outside the trench

Conclusions

- Data from the constant rate test proved that trench construction was viable
- Linear and radial zones of influence were obtainable and sustainable
- Regulators concurred
- Increasing pump size and collection infrastructure to accommodate higher flow/yield

Questions?





11/01/2007